

# Analytical Mechanics

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# Agenda

- 1 Schedule
- 2 Introduction to Analytical Mechanics
- 3 Illustrative Examples
  - Free fall of a mass
  - Open/Closed link mechanisms
  - Watt's governor
  - Beam deformation
- 4 MATLAB environment
- 5 Summary

# Schedule (tentative)

Introduction	1 week
Variational Principles	2 weeks
MATLAB	2 weeks
Link Mechanisms	2 weeks
Rigid Body Rotation	2 weeks
Elastic Deformation	4 weeks
Inelastic Deformation	2 weeks

## web page

<http://www.ritsumei.ac.jp/~hirai/>

English → Classes → 2023 Analytical Mechanics

or directly

<http://www.ritsumei.ac.jp/~hirai/edu/2023/analyticalmechanics/analyticalmechanics-e.html>

# Newton mechanics vs Lagrange mechanics

## Newton mechanics

### vectors

linear momentum, force, angular momentum, moment, ...

vectors **depend** on coordinate systems

**internal forces** have to be identified and eliminated

**constraints** should be solved explicitly

## Lagrange mechanics

### scalars

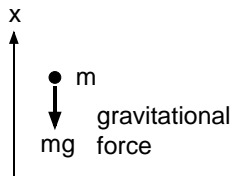
kinetic energy, potential energy, work done by external forces, ...

scalars are **independent** of coordinate systems

**internal forces** do not appear in Lagrangian

**constraints** can be incorporated into Lagrangian

# Free fall of a mass (Newton mechanics)



## Newton mechanics

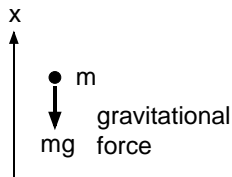
linear momentum  $p = mv$

Newton's eq. of motion  $\frac{dp}{dt} = -mg$

$$\frac{dp}{dt} = \frac{d}{dt}(mv) = m\dot{v}$$

differential equation  $m\dot{v} = -mg$

# Free fall of a mass (Lagrange mechanics)



## Lagrange mechanics

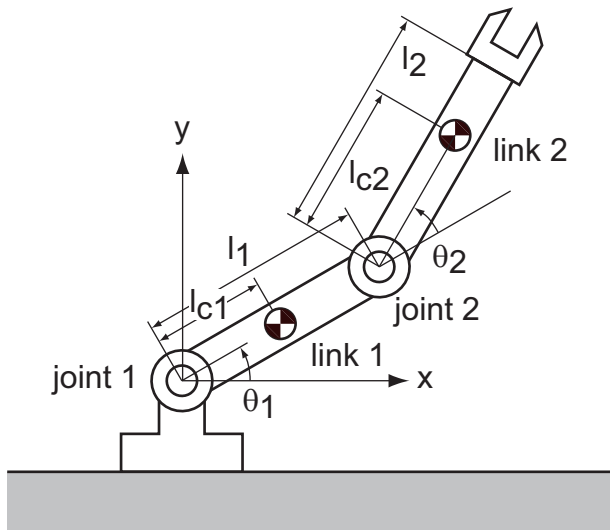
kinetic energy  $T = \frac{1}{2}mv^2$

potential energy  $U = mgx$

Lagrangian  $\mathcal{L} = T - U = \frac{1}{2}mv^2 - mgx$

Lagrange eq. of motion  $\frac{\partial \mathcal{L}}{\partial x} - \frac{d}{dt} \left( \frac{\partial \mathcal{L}}{\partial v} \right) = -mg - m\dot{v} = 0$

# Open link mechanism



# Open link mechanism

## Newton mechanics

- 1 identify all forces applied to each link (inc. internal forces)
- 2 apply Newton's eqs. of motion (and Euler's eqs. of rotation)

$$m_1 \dot{\mathbf{v}}_1 = m_1 \mathbf{g} + \mathbf{R}^{1,0} + \mathbf{R}^{1,2}, \quad m_2 \dot{\mathbf{v}}_2 = m_2 \mathbf{g} + \mathbf{R}^{2,1}, \quad \dots$$

- 3 eliminate internal forces  $\mathbf{R}^{1,0}, \mathbf{R}^{1,2}, \mathbf{R}^{2,1}$

## Lagrange mechanics

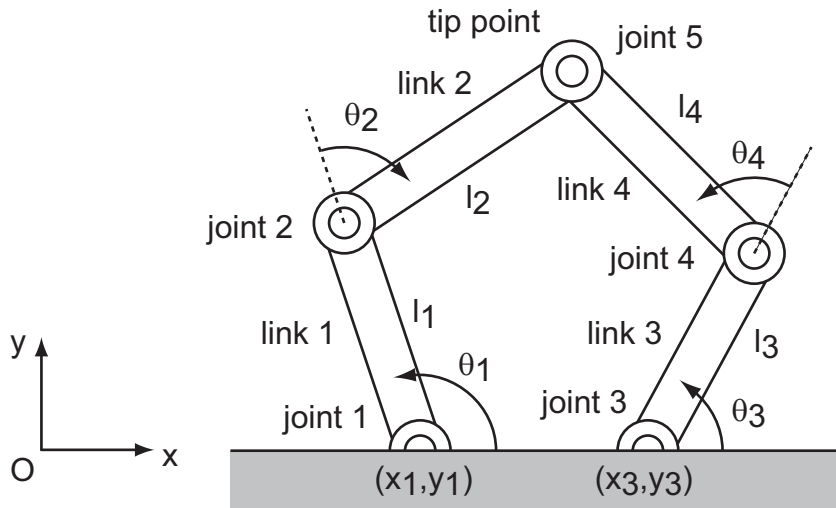
- 1 formulate kinetic and potential energies

$$T = T_1 + T_2, \quad U = U_1 + U_2$$

- 2 apply Lagrange's eqs. of motion to Lagrangian  $\mathcal{L} = T - U$



# Closed link mechanism



# Closed link mechanism

left arm    link 1 – link 2  $\Rightarrow$  open link mech.  $\Rightarrow$  Lagrangian  $\mathcal{L}_{\text{left}}$

right arm    link 3 – link 4  $\Rightarrow$  open link mech.  $\Rightarrow$  Lagrangian  $\mathcal{L}_{\text{right}}$

## geometric constraints

tip position of left arm = tip position of right arm

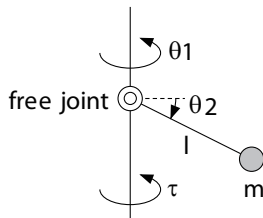
$$X \triangleq l_1 C_1 + l_2 C_{1+2} - l_3 C_3 - l_4 C_{3+4} + x_1 - x_3 = 0$$

$$Y \triangleq l_1 S_1 + l_2 S_{1+2} - l_3 S_3 - l_4 S_{3+4} + y_1 - y_3 = 0$$

## Lagrangian

$$\mathcal{L} = \mathcal{L}_{\text{left}} + \mathcal{L}_{\text{right}} + \lambda_x X + \lambda_y Y$$

# Watt's governor (Newton mechanics)



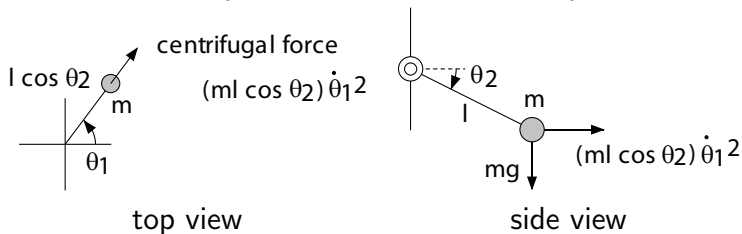
rotation around driving axis

$$I_1 = m(l \cos \theta_2)^2 = ml^2 \cos^2 \theta_2$$

$$\tau = \frac{d}{dt}(I_1 \dot{\theta}_1) = \dot{I}_1 \dot{\theta}_1 + I_1 \ddot{\theta}_1$$

$$\tau = \left\{ ml^2 \cdot 2 \cos \theta_2 (-\sin \theta_2) \dot{\theta}_2 \right\} \dot{\theta}_1 + \left\{ ml^2 \cos^2 \theta_2 \right\} \ddot{\theta}_1$$

# Watt's governor (Newton mechanics)



## rotation around free-joint axis

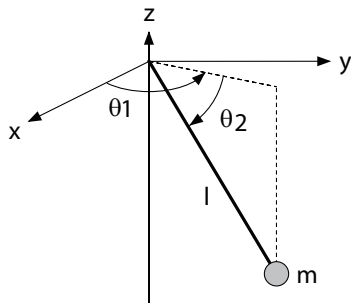
$$I_2 = ml^2$$

$$\frac{d}{dt}(I_2 \dot{\theta}_2) = mg \times l \cos \theta_2 - ml \cos \theta_2 \dot{\theta}_1^2 \times l \sin \theta_2$$

$$ml^2 \ddot{\theta}_2 = mgl \cos \theta_2 - ml^2 \cos \theta_2 \sin \theta_2 \dot{\theta}_1^2$$

need to identify centrifugal force

# Watt's governor (Lagrange mechanics)



position of mass

$$\mathbf{x} = \begin{bmatrix} l \cos \theta_1 \cos \theta_2 \\ l \sin \theta_1 \cos \theta_2 \\ -l \sin \theta_2 \end{bmatrix} = l \begin{bmatrix} \cos \theta_1 \cos \theta_2 \\ \sin \theta_1 \cos \theta_2 \\ -\sin \theta_2 \end{bmatrix}$$

# Watt's governor (Lagrange mechanics)

velocity of mass

$$\begin{aligned}\mathbf{v} &= \frac{d\mathbf{x}}{dt} = \frac{\partial \mathbf{x}}{\partial \theta_1} \frac{d\theta_1}{dt} + \frac{\partial \mathbf{x}}{\partial \theta_2} \frac{d\theta_2}{dt} \\ &= l\dot{\theta}_1 \begin{bmatrix} -\sin \theta_1 \cos \theta_2 \\ \cos \theta_1 \cos \theta_2 \\ 0 \end{bmatrix} + l\dot{\theta}_2 \begin{bmatrix} -\cos \theta_1 \sin \theta_2 \\ -\sin \theta_1 \sin \theta_2 \\ -\cos \theta_2 \end{bmatrix} \\ v^2 &= (l\dot{\theta}_1)^2 \cdot \cos^2 \theta_2 + (l\dot{\theta}_2)^2 \cdot 1 + 2(l\dot{\theta}_1)(l\dot{\theta}_2) \cdot 0 \\ &= l^2(\cos^2 \theta_2 \dot{\theta}_1^2 + \dot{\theta}_2^2)\end{aligned}$$

kinetic/potential energies, work done by external torque

$$T = \frac{1}{2}ml^2(\cos^2 \theta_2 \dot{\theta}_1^2 + \dot{\theta}_2^2), \quad U = -mgl \sin \theta_2, \quad W = \tau \theta_1$$

# Watt's governor (Lagrange mechanics)

## Lagrangian

$$\mathcal{L} \triangleq T - U + W$$

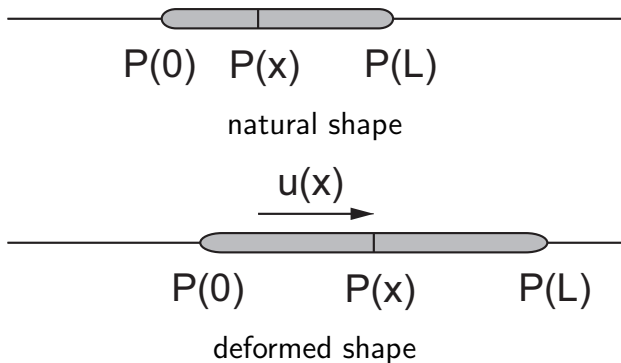
## Lagrange eqs. of motion

$$\frac{\partial \mathcal{L}}{\partial \theta_k} - \frac{d}{dt} \left( \frac{\partial \mathcal{L}}{\partial \dot{\theta}_k} \right) = 0, \quad (k = 1, 2)$$

$$\begin{aligned} \tau - \left\{ ml^2 \cdot 2 \cos \theta_2 (-\sin \theta_2) \dot{\theta}_2 \right\} \dot{\theta}_1 - \left\{ ml^2 \cos^2 \theta_2 \right\} \ddot{\theta}_1 &= 0 \\ -ml^2 \cos \theta_2 \sin \theta_2 \dot{\theta}_1^2 + mgl \cos \theta_2 - ml^2 \ddot{\theta}_2 &= 0 \end{aligned}$$

centrifugal or Coriolis terms yield naturally

# Beam deformation



Deformation is described by **function  $u(x)$**  ( $0 \leq x \leq L$ )



# Beam deformation

## elastic potential energy

$$U = \int_0^L \frac{1}{2} EA \left( \frac{du}{dx} \right)^2 dx$$

## piecewise linear approximation

dividing interval  $[0, L]$  into 6 regions:

$$\int_0^L dx = \int_{x_0}^{x_1} dx + \int_{x_1}^{x_2} dx + \cdots + \int_{x_5}^{x_6} dx$$

linear approximation:

$$\int_{x_i}^{x_j} \frac{1}{2} EA \left( \frac{du}{dx} \right)^2 dx \approx \frac{1}{2} \begin{bmatrix} u_i & u_j \end{bmatrix} \frac{EA}{h} \begin{bmatrix} 1 & -1 \\ -1 & 1 \end{bmatrix} \begin{bmatrix} u_i \\ u_j \end{bmatrix}$$

# Beam deformation

elastic potential energy

$$U = \frac{1}{2} \begin{bmatrix} u_0 & u_1 & \cdots & u_6 \end{bmatrix} \frac{EA}{h} \begin{bmatrix} 1 & -1 & & & & & \\ -1 & 2 & -1 & & & & \\ & \ddots & \ddots & \ddots & & & \\ & & & -1 & 2 & -1 & \\ & & & & -1 & 1 & \end{bmatrix} \begin{bmatrix} u_0 \\ u_1 \\ \vdots \\ u_5 \\ u_6 \end{bmatrix}$$

Deformation is described by a finite number of variables  $u_0$  through  $u_6$   
finite element method (FEM)

# What is MATLAB?

- ① Software for numerical calculation
- ② can handle vectors or matrices directly
- ③ Functions such as ODE solvers and optimization
- ④ Toolboxes for various applications
- ⑤ both programming and interactive calculation

# What is MATLAB?

## MATLAB environment

MATLAB Total Academic Headcount (TAH)

MATLAB with all toolboxes is available

## Information

<https://it.support.ritsumeai.ac.jp/hc/ja>

# What is MATLAB?

- Install MATLAB into your own PC or mobile
- Sample programs are on the web of the class
- You can use your own PC or mobile in class

# Summary: pros & cons of Lagrange mechanics

## Pros

- scalar description
- once energies and works are formulated, derivative calculation yields equations of motion directly
- do not have to introduce internal forces
- effective for complex systems, such as link mechanisms, rotating or deforming objects

## Cons

- difficult to understand the derived equation intuitively
- all non-potential forces, such as friction and viscous forces, are treated as external forces